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Method for depletion of sulphur and/or compounds containing sulphur from a biochemically produced organic compound

## Description

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The present invention relates to a method of reducing the concentration of sulfur and/or sulfur-containing compounds in a biochemically prepared organic compound, ethanol which can be prepared by this method and its use.

There is an increasing demand for biochemically prepared chemical compounds, e.g. compounds prepared by fermentation, as, for example, building blocks in the chemical synthesis of high-value chemicals or as "green" fuels.

(Cf., for example, H. van Bekkum et al., Chem. for Sustainable Development 11, 2003, pages 11-21).

Examples of these renewable resources are alcohols such as ethanol, butanol and methanol, diols such as 1,3-propanediol and 1,4-butanediol, triols such as glycerol, carboxylic acids such as lactic acid, acetic acid, propionic acid, citric acid, butyric acid, formic acid, malonic acid and succinic acid.

- In place of synthetic ethanol, which is produced predominantly by hydration of ethylene, ethanol from biological sources, known as bioethanol, can also be used for many applications.
- Instead of synthetic 1,3-propanediol, which is predominantly prepared by hydrolysis of acrolein to 3-hydroxypropanal in the presence of an acid catalyst followed by metal-catalyzed hydrogenation or by hydroformylation of ethylene oxide (Industrial Organic Chemistry, Weissermel and Arpe, 2003), 1,3-propanediol from biological sources, known as bio-1,3-propanediol, can also be used for many applications (US-A-6,514,733, DE-A-38 29 618).

Instead of synthetic lactic acid prepared by hydrolysis of lactonitrile, lactic acid from biological sources can also be used for many applications (K. Weissermel and H.-J. Arpe, Industrial Organic Chemistry, Wiley-VCH, Weinheim, 2003, p. 306).

Edible oils and animal fats can be transesterified to produce biodiesel. In addition to biodiesel, a glycerol fraction is formed in this process. Uses of glycerol comprise applications in the chemical industry, for instance the preparation of pharmaceuticals, cosmetics, polyether isocyanates, glycerol tripolyethers (K. Weissermel and H.-J. Arpe, Industrial Organic Chemistry, Wiley-VCH, Weinheim, 2003, p. 303).

Uses of ethanol comprise applications in the chemical industry, for instance the preparation of ethylamines, the preparation of ethyl esters from carboxylic acids (in particular ethyl acetate), the preparation of butadiene or ethylene, the preparation of ethyl acetate via acetaldehyde and the preparation of ethyl chloride (K. Weissermel and H.-J. Arpe, Industrial Organic Chemistry, Wiley-VCH, Weinheim, 2003), and in the cosmetics and pharmaceuticals industry or in the food industry and also in cleaners, solvents and paints (N. Schmitz, Bioethanol in Deutschland, Landwirtschaftsverlag, Münster, 2003).

Further uses are: feed in steam reforming processes and hydrogen source in fuel cells (S. Velu et al., Cat. Letters 82, 2002, pages 145-52; A.N. Fatsikostas et al., Cat. Today 75, 2002, pages 145-55; F. Aupretre et al., Cat. Commun. 3, 2002, pages 263-67; V. Fierro et al., Green Chem. 5, 2003, pages 20-24; M. Wang, J. of Power Sources 112, 2002, pages 307-321).

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Uses of 1,3-propanediol comprise applications in the chemical industry, for instance the production of pharmaceuticals, polyesters, polytrimethylene terephthalates, fibers.

Uses of lactic acid are in the food industry and in the production of biodegradable polymers.

The use of biochemically prepared compounds such as bioethanol, bio-1,3-propanediol or lactic acid, especially in particularly pure form, would be more advantageous and cheaper in many of these applications.

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The purification or isolation of the biochemically prepared compounds is frequently carried out by distillation in complicated, multistage processes.

However, the advantage of the respective biochemically prepared compound is, as has been recognized according to the invention, frequently decreased by the compound comprising small amounts of sulfur and/or sulfur-containing compounds, in particular specific sulfur compounds, even after the known purification processes and the sulfur or the sulfur-containing compounds frequently interfering in the respective applications.

Thus, the sulfur content of bioethanol interferes in its use in ammination to form ethylamines by poisoning the metal catalyst. A similar situation applies in amminations of other bioalcohols.

The ammination of alcohols is carried out industrially over

hydrogenation/dehydrogenation catalysts, in particular heterogeneous
hydrogenation/dehydrogenation catalysts, by reaction of the respective alcohol with
ammonia, primary or secondary amines at elevated pressure and elevated temperature

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in the presence of hydrogen. C.f., for example, Ullmann's Encyclopedia of Industrial Chemistry, sixth edition, 2000, 'Aliphatic Amines: Production from alcohols'.

The catalysts usually comprise transition metals, for instance metals of groups VIII and IB, often copper, as catalytically active components which are frequently applied to an inorganic support such as aluminum oxide, silicon dioxide, titanium dioxide, carbon, zirconium oxide, zeolites, hydrotalcites and similar materials known to those skilled in the art.

10 If the corresponding bioalcohol is used, the catalytically active metal surface of the heterogeneous catalysts becomes coated with the sulfur or sulfur compounds introduced via the bioalcohol to an increasing extent over time. This leads to accelerated catalyst deactivation and thus to a significant deterioration in the economics of the respective process.

The sulfur content of bioethanol also has an adverse effect due to poisoning of the catalyst, e.g. in steam reforming processes for the production of hydrogen and in fuel cells.

In general, the sulfur content of chemicals derived from natural raw materials will have an adverse effect on a reaction carried out using them, for instance as a result of, as described, metal centers being sulfurized and thereby deactivated, or acidic or basic centers being occupied, secondary reactions occurring or being catalyzed, formation of deposits in production plants and contamination of the products.

A further adverse effect of sulfur and/or sulfur-containing compounds in the biochemically prepared compounds is their typical unpleasant odor which is disadvantageous, in particular, in cosmetic applications, in disinfectants, in foodstuffs and in pharmaceutical products.

It is therefore of great economic interest to reduce the concentration of sulfur and/or sulfur-containing compounds in biochemically prepared organic compounds such as bioethanol, bio-1,3-propanediol, bio-1,4-butanediol, bio-1-butanol (in general: bioalcohols), or to remove the sulfur and/or the sulfur-containing compounds virtually entirely, by means of a desulfurization step preceding their use.

WO-A-2003 020850, US-A1-2003 070966, US-A1-2003 113598 and US-B1-6,531,052 concern the removal of sulfur from liquid hydrocarbons (petroleum spirit).

40 Chemical Abstracts No. 102: 222463 (M.Kh. Annagiev et al., Doklady – Akademiya Nauk Azerbaidzhanskoi SSR, 1984, 40 (12), 53-6) describes decreasing the concentration of S compounds in technical-grade ethanol (not bioethanol) from 25-30

to 8-17 mg/l by bringing the ethanol into contact with zeolites of the clinoptilolite and mordenite types at room temperature, with the zeolites having been conditioned beforehand at 380°C for 6 hours and in some cases treated with metal salts, in particular Fe<sub>2</sub>O<sub>3</sub>. The S compounds removed are H<sub>2</sub>S and alkyl thiols (R-SH).

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It was an object of the present invention to discover an improved economical method of treating biochemically prepared organic compounds such as bioalcohols, e.g. bioethanol, by means of which the corresponding treated compound is obtained in high yield, space-time yield and selectivity and which when used, for example, in chemical synthetic processes such as the preparation of ethylamines, in particular monoethylamine, diethylamine and triethylamine, from bioethanol, and also in other applications, e.g. in the chemical, cosmetic or pharmaceutical industry or in the food industry, has improved properties.

In particular, the use of a treated bioethanol should make increased catalyst operating lifes in the synthesis of ethylamines possible.

(Space-time yields are reported in 'amount of product/(catalyst volume ● time)' (kg/(l<sub>cat.</sub> ● h)) and/or 'amount of product/(reactor volume ● time)' (kg/(l<sub>reactor</sub> ● h)).

We have accordingly found a method of reducing the concentration of sulfur and/or a sulfur-containing compound in a biochemically prepared organic compound, which comprises bringing the respective organic compound into contact with an adsorbent.

Furthermore, ethanol which has a particular specification (see below) and can be prepared by the abovementioned method and its use as solvent, disinfectant, as component in pharmaceutical or cosmetic products or in foodstuffs or in cleaners, as feed in steam reforming processes for the synthesis of hydrogen or in fuel cells or as building block in chemical synthesis has been found.

The method of the invention is particularly useful for reducing the concentration of sulfur or a sulfur-containing compound in a compound prepared by fermentation.

The sulfur-containing compounds are inorganic or organic compounds, in particular symmetrical or unsymmetrical  $C_{2-10}$ -dialkyl sulfides, particularly  $C_{2-6}$ -dialkyl sulfides such as diethyl sulfide, di-n-propyl sulfide, diisopropyl sulfide, very particularly dimethyl sulfide,  $C_{2-10}$ -dialkyl sulfoxides such as dimethyl sulfoxide, diethyl sulfoxide, dipropyl sulfoxide, 3-methylthio-1-propanol and/or S-containing amino acids such as methionine and S-methylmethionine.

The biochemically prepared organic compound is preferably an alcohol, ether or a carboxylic acid, in particular ethanol, 1,3-propanediol, 1,4-butanediol, 1-butanol,

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glycerol, tetrahydrofuran, lactic acid, succinic acid, malonic acid, citric acid, acetic acid, propionic acid, 3-hydroxypropionic acid, butyric acid, formic acid or gluconic acid.

As adsorbents, preference is given to using a silica gel, an activated aluminum oxide, a zeolite having hydrophilic properties, an activated carbon or a carbon molecular sieve.

Examples of silica gels which can be used are silicon dioxide, examples of aluminum oxides which can be used are boehmite, gamma-, delta-, theta-, kappa-, chi- and alpha-aluminum oxide, examples of activated carbons which can be used are carbons produced from wood, peat, coconut shells, or synthetic carbons and carbon blacks produced, for instance, from natural gas, petroleum or downstream products, or polymeric organic materials which can also comprise heteroatoms such as nitrogen, and examples of carbon molecular sieves which can be used are molecular sieves produced from anthracite and hard coal by partial oxidation, and these are described, for example, in the electronic version of the sixth edition of Ullmann's Encyclopedia of Industrial Chemistry, 2000, Chapter Adsorption, Paragraph 'Adsorbents'.

If the adsorbent is produced as shaped bodies, for instance for a fixed-bed process, it can be used in any desired shape. Typical shaped bodies are spheres, extrudates, hollow extrudates, star extrudates, pellets, crushed material, etc., having characteristic diameters of from 0.5 to 5 mm, or monolites and similar structured packing elements (cf. Ullmann's Encyclopedia, sixth edition, 2000 Electronic Release, Chapter Fixed-Bed Reactors, Par. 2: Catalyst Forms for Fixed-Bed Reactors).

In the case of a suspension procedure, the adsorbent is used in powder form. Typical particle sizes in such powders are 1–100 µm, but it is also possible to use particles significantly smaller than 1 µm, for instance when using carbon black. The filtration in suspension processes can be carried out batchwise, for instance by deep bed filtration. In continuous processes, crossflow filtration, for example, is a possibility.

Adsorbents used are preferably zeolites, in particular zeolites from the group consisting of natural zeolites, faujasite, X-zeolite, Y-zeolite, A-zeolite, L-zeolite, ZSM 5 zeolite, ZSM 8 zeolite, ZSM 11 zeolite, ZSM 12 zeolite, mordenite, beta-zeolite, pentasil zeolite and mixtures thereof which contain ion-exchangeable cations.

Such zeolites, including commercial zeolites, are described in Kirk-Othmer Encyclopedia of Chemical Engineering 4th Ed. Vol 16. Wiley, NY, 1995, and also, for example, in Catalysis and Zeolites, J. Weitkamp and L. Puppe, Eds, Springer, Berlin (1999).

It is also possible to use metal organic frameworks (MOFs) (e.g. Li et al., Nature, 402, 1999, pages 276-279).

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The cations of the zeolite, e.g. H<sup>+</sup> in the case of a zeolite in the H form or Na<sup>+</sup> in the case of a zeolite in the Na form, are preferably completely or partly replaced by metal cations, in particular transition metal cations. (Loading of the zeolites with metal cations).

This can be carried out by, for example, ion exchange, impregnation or evaporation of soluble salts. However, the metals are preferably applied to the zeolite by ion exchange, since they then have, as recognized according to the invention, a particularly high dispersion and thus a particularly high sulfur adsorption capacity. Cation exchange can be carried out, for example, starting from zeolites in the alkali metal, H or ammonium form. In Catalysis and Zeolites, J. Weitkamp and L. Puppe, Eds., Springer, Berlin (1999), such ion exchange techniques for zeolites are described comprehensively.

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Preferred zeolites have a modulus (molar SiO<sub>2</sub>:Al<sub>2</sub>O<sub>3</sub> ratio) in the range from 2 to 1000, in particular from 2 to 100.

Very particular preference is given to using adsorbents, in particular zeolites,
comprising one or more transition metals, in elemental or cationic form, from groups
VIII and IB of the Periodic Table, e.g. Fe, Co, Ni, Ru, Rh, Pd, Os, Ir, Pt, Cu, Ag and/or
Au, preferably Ag and/or Cu, in the method of the invention.

The adsorbent preferably comprises from 0.1 to 75% by weight, in particular from 1 to 60% by weight, particularly preferably from 2 to 50% by weight, very particularly preferably from 5 to 30% by weight, (in each case based on the total mass of the adsorbent) of the metal or metals, in particular the transition metal or transition metals.

Processes for preparing such metal-containing adsorbents are known to those skilled in the art, e.g. from Larsen et al., J. Chem. Phys. 98, 1994 pages 11533-11540 and J. Mol. Catalysis A, 21 (2003) pages 237-246.

In Catalysis and Zeolites, J. Weitkamp and L. Puppe, Eds, Springer, Berlin (1999), ion exchange techniques for zeolites are described comprehensively.

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For example, A.J. Hernandez-Maldonado et al. in Ind. Eng. Chem. Res. 42, 2003, pages 123-29, describe a suitable method for preparing an Ag-Y-zeolite by ion exchange of Na-Y-zeolite with an excess of silver nitrate in aqueous solution (0.2 molar) at room temperature over 24-48 hours. After the ion exchange, the solid is isolated by filtration, washed with large amounts of deionized water and dried at room temperature.

In addition, T.R. Felthouse et al., J. of Catalysis 98, pages 411-33 (1986), for example, describe the preparation of the respective Pt-containing zeolites from the H forms of Yzeolite, mordenite and ZSM-5.

5 The methods disclosed in WO-A2-03/020850 for preparing Cu-Y- and Ag-Y-zeolites by ion exchange from Na-Y-zeolites are also suitable for obtaining adsorbents preferred for the method of the invention.

Very particularly preferred adsorbents are:

- Ag-X-zeolite having an Ag content of from 10 to 50% by weight (based on the total mass of the adsorbent) and Cu-X-zeolite having a Cu content of from 10 to 50% by weight (based on the total mass of the adsorbent).
- To carry out the method of the invention, the adsorbent is generally brought into contact with the organic compound at temperatures in the range from 0°C to 200°C, in particular from 10°C to 50°C.
- The contacting with the adsorbent is preferably carried out at an absolute pressure in the range from 1 to 200 bar, in particular from 1 to 5 bar.
  - It is particularly preferably carried out at room temperature and under atmospheric pressure.
- In a preferred embodiment of the method of the invention, the respective organic compound is brought into contact with the adsorbent in the liquid phase, i.e. in liquid form or dissolved or suspended in a solvent or diluent.
- Possible solvents are, in particular, those which are able to dissolve the compounds to be purified virtually completely or are completely miscible with these and are inert under the process conditions.
- Examples of suitable solvents are water, cyclic and alicyclic ethers, e.g. tetrahydrofuran, dioxane, methyl tert-butyl ether, dimethoxyethane, dimethoxypropane, dimethyl diethylene glycol, aliphatic alcohols such as methanol, ethanol, n-propanol or isopropanol, n-butanol, 2-butanol, isobutanol or tert-butanol, carboxylic esters such as methyl acetate, ethyl acetate, propyl acetate or butyl acetate, and also aliphatic ether alcohols such as methoxypropanol.
- The concentration of the compound to be purified in the liquid, solvent-containing phase can in principle be chosen freely and is frequently in the range from 20 to 95% by weight, based on the total weight of the solution/mixture.

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One variant of the method of the invention comprises carrying it out in the presence of hydrogen under atmospheric pressure or superatmospheric pressure.

- The method can be carried out in the gas or liquid phase, in the fixed-bed or suspension mode, with or without backmixing, continuously or batchwise according to the methods known to those skilled in the art (e.g. as described in Ullmann's Encyclopedia, sixth edition, 2000 electronic release, Chapter "Adsorption").
- To obtain a very high reduction in the concentration of the sulfur compound, processes having a low degree of backmixing are particularly useful.

The method of the invention makes it possible, in particular, to reduce the concentration of sulfur and/or sulfur-containing compounds in the respective compound by  $\geq 90\%$  by weight, particularly preferably  $\geq 95\%$  by weight, very particularly preferably  $\geq 98\%$  by weight (in each case calculated as S).

The method of the invention makes it possible, in particular, to reduce the concentration of sulfur and/or sulfur-containing compounds in the respective compound to a residual content of < 2 ppm by weight, particularly preferably < 1 ppm by weight, very particularly preferably from 0 to < 0.1 ppm by weight (in each case calculated as S), for example determined by the Wickbold method (DIN EN 41).

The bioethanol which is preferably used in the method of the invention is generally produced from agricultural products such as molasses, cane sugar juice, maize starch or from products of wood saccharification and from sulfite waste liquors by fermentation.

Preference is given to using bioethanol which has been obtained by fermentation of glucose with elimination of CO<sub>2</sub> (K. Weissermel and H.-J. Arpe, Industrial Organic Chemistry, Wiley-VCH, Weinheim, 2003, p. 194; Electronic Version of Sixth Edition of Ullmann's Encyclopedia of Industrial Chemistry, 2000, Chapter Ethanol, Paragraph Fermentation). The ethanol is generally isolated from the fermentation broths by distillation methods: Electronic Version of Sixth Edition of Ullmann's Encyclopedia of Industrial Chemistry, 2000, Chapter Ethanol, Paragraph Recovery and Purification.

According to the invention, the ethanol prepared using the method found is advantageously used

40 as building block in chemical synthesis, e.g.

in processes (known to those skilled in the art) for preparing a primary, secondary or tertiary ethylamine, a monoethylamine or diethylamine, in particular monoethylamine, diethylamine and/or triethylamine, by reacting the ethanol with NH<sub>3</sub>, a primary amine or a secondary amine in the presence of hydrogen at elevated temperatures and pressures in the presence of a heterogeneous catalyst comprising a metal of group VIII and/or IB of the Periodic Table,

in processes (known to those skilled in the art) for preparing an ethyl ester, in particular by esterification of ethanol with a carboxylic acid or transesterification of a carboxylic ester with ethanol,

in processes (known to those skilled in the art) for preparing ethylene by dehydration,

as solvent, disinfectant, and

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as component in pharmaceutical or cosmetic products or in foodstuffs or in cleaners, as feed in steam reforming processes for the synthesis of hydrogen or in fuel cells.

The present invention also provides an ethanol which can be prepared using the method of the invention and has

a content of sulfur and/or sulfur-containing organic compounds in the range from 0 to 2 ppm by weight, preferably from 0 to 1 ppm, particularly preferably from 0 to 0.1 ppm (in each case calculated as S), for example determined by the Wickbold method (DIN EN 41).

a content of C<sub>3-4</sub>-alkanols in the range from 1 to 5000 ppm by weight, preferably from 5 to 3000 ppm by weight, particularly preferably from 10 to 2000 ppm by weight,

a methanol content in the range from 1 to 5000 ppm by weight, preferably from 5 to 3000 ppm by weight, particularly preferably from 10 to 2000 ppm by weight,

an ethyl acetate content in the range from 1 to 5000 ppm by weight, preferably from 5 to 3000 ppm by weight, particularly preferably from 10 to 2000 ppm by weight, and

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a 3-methyl-1-butanol content in the range from 1 to 5000 ppm by weight, preferably from 5 to 3000 ppm by weight, particularly preferably from 10 to 2000 ppm by weight.

The content of C<sub>3-4</sub>-alkanols, methanol, ethyl acetate and 3-methyl-1-butanol is, for example, determined by means of gas chromatography (30m DB-WAX column, internal diameter: 0.32 mm, film thickness: 0.25 μm, FID, temperature program: 35°C (5 min), 10°C/min, heating rate: 200°C (8 min.).

Examples

Preparation of Ag-zeolites

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Example 1: Ag-zeolite powder

A solution of  $AgNO_3$  (7.71 g of  $AgNO_3$  in water, 200 ml total) was placed in a glass beaker, the zeolite (ZSM-5, 200 g, molar  $SiO_2/Al_2O_3$  ratio = 40-48, Na form) was slowly added while stirring and the mixture was stirred at room temperature for 2 hours. The adsorbent was then filtered off via a fluted filter. The adsorbent was subsequently dried at 120°C for 16 hours in a dark drying oven. The adsorbent comprised 2.1% by weight of Ag (based on the total mass of the adsorbent).

## 15 Example 2: Ag-zeolite shaped bodies

A solution of AgNO<sub>3</sub> (22.4 g in water, 100 ml total) was placed in a glass beaker. The zeolite (65 g of molar sieve 13X in the form of spheres having a diameter of 2.7 mm, molar SiO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> ratio = 2, Na form) was placed in the apparatus. 400 ml of water were then introduced and were circulated by pumping at room temperature in a continuous plant. The silver nitrate solution was added dropwise over a period of 1 hour. The mixture was then circulated by pumping overnight (23 h). The adsorbent was then washed free of nitrate with 12 liters of deionized water and was subsequently dried overnight at 120°C in a dark drying oven. The adsorbent comprised 15.9% by weight of Ag (based on the total mass of the adsorbent).

#### Example A

All ppm figures in this document are by weight.

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To test the desulfurization, 10 g of the adsorbent (cf. the table below) was in each case baked overnight at 150°C in a drying oven to remove adsorbed water. After the solid had cooled, it was taken from the drying oven and 300 ml of ethanol (absolute ethanol, > 99.8%, source: Riedel de Haën) were poured over it. About 17 ppm of dimethyl sulfide (corresponds to about 9 ppm of sulfur) had been added to the ethanol, since preliminary experiments showed that dimethyl sulfide is a sulfur compound representative of the organic sulfur compounds present in bioethanol.

The Ag/ZSM-5 adsorbent was prepared by ion exchange of the Na-ZSM-5 with an aqueous AgNO<sub>3</sub> solution (50 g of ZSM-5, 1.94 g of AgNO<sub>3</sub>, 50 ml of impregnation solution). A commercially available ZSM-5 (molar SiO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> ratio = 40-48, Na form,

ALSI-PENTA®) was used for this purpose. The catalyst was subsequently dried at 120°C.

The Ag/SiO<sub>2</sub> adsorbent was prepared by impregnating SiO<sub>2</sub> (BET about 170 m<sup>2</sup>/g, Na<sub>2</sub>O content: 0.4% by weight) with an aqueous AgNO<sub>3</sub> solution (40 g of SiO<sub>2</sub>, 1.6 g of AgNO<sub>3</sub>, 58 ml of impregnation solution). The catalyst was subsequently dried at 120°C and calcined at 500°C.

The Ag/Al<sub>2</sub>O<sub>3</sub> adsorbent was prepared by impregnating gamma-Al<sub>2</sub>O<sub>3</sub> (BET about 220 m<sup>2</sup>/g) with an aqueous AgNO<sub>3</sub> solution (40 g of Al<sub>2</sub>O<sub>3</sub>, 1.6 g of AgNO<sub>3</sub>, 40 ml of impregnation solution). The catalyst was subsequently dried at 120°C and calcined at 500°C.

The ethanol/adsorbent suspension was transferred to a 4-neck glass flask into which nitrogen was passed for about 5 minutes to make it inert. The flask was subsequently closed and the suspension was stirred at room temperature for 5 hours. After the experiment, the adsorbent was filtered off by means of a fluted filter. The sulfur content of the filtrate and, if appropriate, of the adsorbent was determined coulometrically:

Adsorbent	S content/p	pm		
	Input	Output	Fresh adsorbent	Laden adsorbent
Ag/ZSM-5	9	< 2	25	230
ZSM-5	9	4	n.d.	n.d.
Ag/Al <sub>2</sub> O <sub>3</sub>	9	2	n.d.	n.d.
Ag/SiO <sub>2</sub>	9	4	n.d.	n.d.

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(n.d. = not determined)

The table shows that the silver-laden zeolite in particular was able to reduce the sulfur content to values below the detection limit (= 2 ppm).

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After the same Ag/ZSM-5 sample had been used three times, < 2 ppm of sulfur were detected in the ethanol after carrying out the experiment.

Even in the case of the adsorbent in which silver had been applied to other supports such as Al<sub>2</sub>O<sub>3</sub> or SiO<sub>2</sub>, desulfurization was observed. Even the undoped zeolite led to some removal of sulfur from the ethanol. The best result was obtained using the silver-doped zeolite.

Other materials such as Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst or Ni catalyst were also suitable for removing S from bioethanol, but not as good as the silver-doped zeolite even when the treatment was carried out at elevated temperature with addition of hydrogen.

#### 5 Examples B

#### Example B1

To test the desulfurization, 20 g of the pulverulent adsorbent Ag-ZSM5, 2.1% by weight of Ag, was used (cf. Example 1) and 300 ml of ethanol (absolute ethanol, > 99.8%, source: Riedel de Haën) were poured over it. About 175 ppm of dimethyl sulfide (> 99%, Merck) (corresponds to about 90 ppm of sulfur) had been added to the ethanol, since preliminary experiments showed that dimethyl sulfide is a sulfur compound representative of the organic sulfur compounds present in bioethanol. The ethanol/adsorbent suspension was transferred to a closed 4-neck glass flask. The suspension was stirred at room temperature and atmospheric pressure. After the experiment, the adsorbent was filtered off via a fluted filter. The sulfur content of the input, filtrate and, if appropriate, the adsorbent was determined coulometrically. The same Ag-ZSM5 sample was used another three times:

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Use	Residence	Input	Output	Laden adsorbent
	time	S ppm	S ppm	S ppm
	Hours			
1	5	84	<2	1300
2	24	84	<2	2800
3	24	95	10	4600
4	24	97	29	5900

#### Example B2

To test the desulfurization, 300 ml of ethanol (absolute ethanol, > 99.8%, Riedel de
25 Haën) were poured over pulverulent desulfurization materials. About 175 ppm of
dimethyl sulfide (> 99%, Merck) (corresponds to about 90 ppm of sulfur) had been
added to the ethanol. The ethanol/adsorbent suspension was transferred to a closed 4neck glass flask. The suspension was stirred at room temperature and atmospheric
pressure for 24 hours. After the experiment, the adsorbent was filtered off via a fluted
30 filter. The sulfur content of the input, filtrate and, if appropriate, the adsorbent was
determined coulometrically.

Adsorbent	Adsorben	Input	Output	Laden adsorbent
	t	S ppm	S ppm	S ppm
	% by			
	weight			
40 CuO/40 ZnO/20 Al <sub>2</sub> O <sub>3</sub> , in %	8.5	84	64	22
by weight				
17 NiO/ 15 SiO <sub>2</sub> /5 Al <sub>2</sub> O <sub>3</sub> / 5	8.5	95	58	9
ZrO <sub>2</sub> , in % by weight				
5% by weight Pd/C	2.5	100	39	2300
2nd use of the Pd/C adsorbent		97	60	3000

The materials CuO-ZnO/Al<sub>2</sub>O<sub>3</sub> and NiO/SiO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub>/ZrO<sub>2</sub> are suitable for desulfurization, but are not as good as, for example, a silver-doped zeolite, even when the treatment was carried out at elevated temperature and with addition of hydrogen. If palladium on carbon is used, sulfur is taken up from ethanol.

#### Example B3

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To test the adsorbent, a continuous fixed-bed plant having a total volume of 192 ml
was charged with 80.5 g of Ag-13X spheres (15.9% by weight of Ag, 2.7 mm spheres,
described in Example 2). About 80 ppm of dimethyl sulfide (> 99%, Merck)
(corresponds to about 40 ppm of sulfur) were added to the feed ethanol (absolute
ethanol, > 99.8%, Riedel de Haën). The feed was passed over the adsorbent in the
upflow mode. During sampling, the sample flask was always cooled in an ice/salt
mixture.

Time of operation	Cumulative loading (ppm of S/g of adsorbent)	Input S ppm	Output S ppm
24	934	38	<2
48	1623	41	<2
72	2222	42	<2

The determination of sulfur in the input and output was carried out (in all examples) coulometrically (DIN 51400 Part 7) with a detection limit of 2 ppm.

## Example B4

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To test the desulfurization, 500 ml of ethanol (absolute ethanol, > 99.8%, Riedel de Haën) were in each case poured over 4 g of the adsorbent (cf. the table below). About 390 ppm of dimethyl sulfide (> 99%, Merck) (corresponds to about 200 ppm of sulfur) had been added to the ethanol.

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The preparation of Ag-13X is described in Example 1. CBV100 and CBV720 are zeolite-Y systems. The doping with metals was carried out by cation exchange in a manner analogous to Example 1 using AgNO<sub>3</sub> or CuNO<sub>3</sub> solutions. The Cu-CPV720 was subsequently calcined at 450°C in N<sub>2</sub>.

The ethanol/adsorbent suspension was transferred to a 4-neck glass flask and stirred at room temperature under atmospheric pressure for 24 hours. After the experiment, the adsorbent was filtered off via a fluted filter. The sulfur content of the filtrate and, if appropriate, of the adsorbent was determined coulometrically:

Adsorbent		S contents/ppm				
	Form	Input	Output	Laden adsorbent		
None	-	200	170	-		
Ag-13X	Spheres (2.7 mm)	200	96	n.d.		
Ag-CBV100	Powder	190	13	18000		
Ag-CBV720	Powder	190	77	n.d.		
Cu-CBV720	Powder	190	97	390		

(n.d. = not determined)

The table shows that both silver-doped zeolites and copper-doped zeolites are able to desulfurize ethanol.

Example

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20 Various commercial bioethanol grades were analyzed to determine their sulfur content.

	Bio-						
	EtOH 1	EtOH 2	EtOH 3	EtOH 4	EtOH 5	EtOH 6	EtOH 7
Total S	0.6	1	0.6	8	2	49	2
(ppm by weight)							
Sulfate S	0.33	0.43	0.2	n.d.	0.9	6	2
(ppm by weight)							

Total S = Total sulfur, determined coulometrically in accordance with DIN 51400 Part 7

Total sulfur contents ≤ 2 ppm were determined by the Wickbold method (DIN EN 41)

Sulfate S = Sulfate sulfur, determined by ion chromatography using a method analogous to that of EN ISO 10304-2